

Advanced Parameters in HEC-RAS

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Overview

- Turbulence
 - Overview of Theory
 - Numerical Implementation
 - Example
 - Guidance and Best Practices
- Coriolis
 - Overview of Theory
 - Numerical Implementation
 - Guidance and Best Practices
- Matrix Solvers
 - Direct vs. Iterative Solvers
 - Iterative Solver Input Parameters
 - Example
 - Guidance and Best Practices



HEC-RAS Turbulence Modeling

- Turbulence is a type of fluid flow which is unsteady, irregular in space and time, dissipative, and diffusive.
- Most natural flows are turbulent
- Dispersion is due to the non-uniform velocity distribution
- Turbulence and dispersion are represented with a diffusion term in the momentum equations
- Two aspects (both changed for Version 6.0)
 1. Formulation in momentum equations
 2. Eddy viscosity formulation (aka “turbulence model”)



Momentum Equations: Diffusion Term

- Non-conservative Formulation
 - Only option in Versions 5.0.7 and earlier
 - Still in option in Version 6.0

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - fv = -g \frac{\partial H}{\partial x} + v_t \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right) - c_f u$$

$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + fu = -g \frac{\partial H}{\partial y} + v_t \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) - c_f v$$

- Conservative Formulation

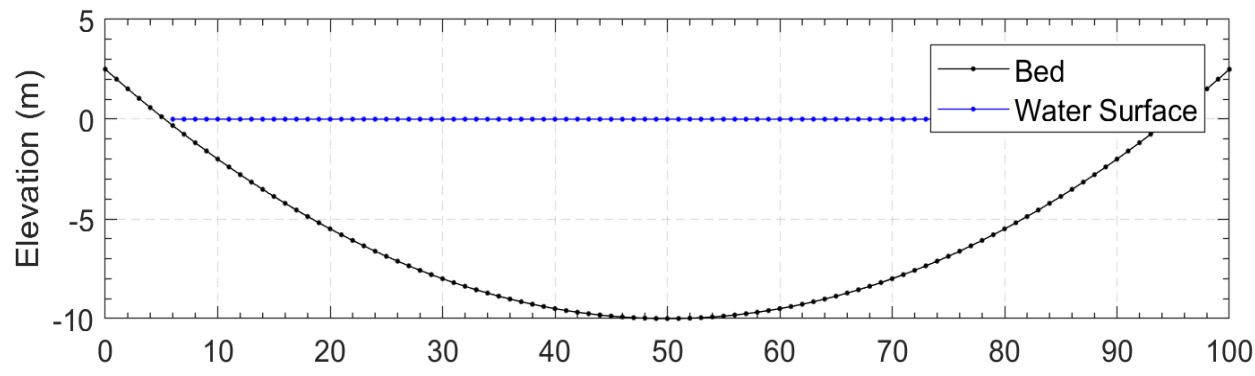
- New for Version 6.0

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} - fv = -g \frac{\partial H}{\partial x} + \frac{1}{h} \frac{\partial}{\partial x} \left(v_{t,xx} h \frac{\partial u}{\partial x} \right) + \frac{1}{h} \frac{\partial}{\partial y} \left(v_{t,yy} h \frac{\partial u}{\partial y} \right) - c_f u$$

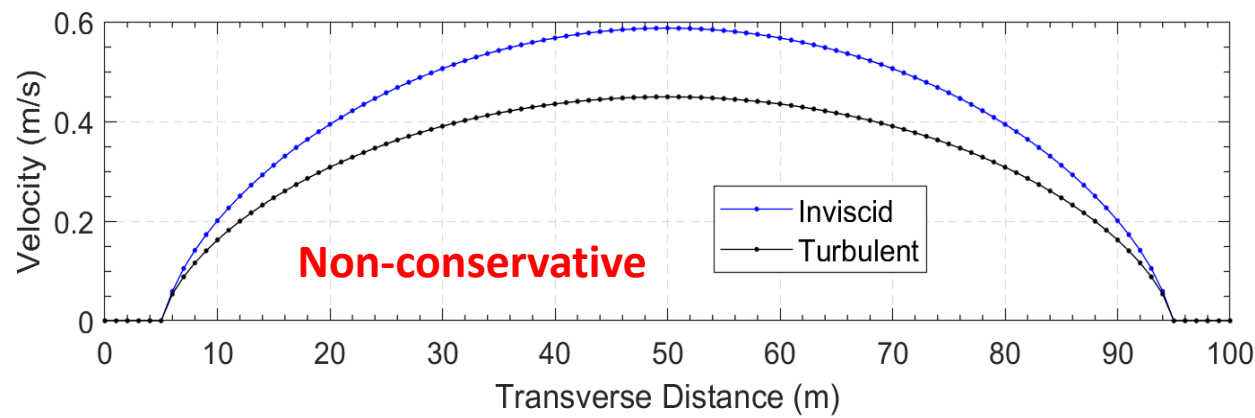
$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + fu = -g \frac{\partial H}{\partial y} + \frac{1}{h} \frac{\partial}{\partial x} \left(v_{t,xx} h \frac{\partial v}{\partial x} \right) + \frac{1}{h} \frac{\partial}{\partial y} \left(v_{t,yy} h \frac{\partial v}{\partial y} \right) - c_f v$$



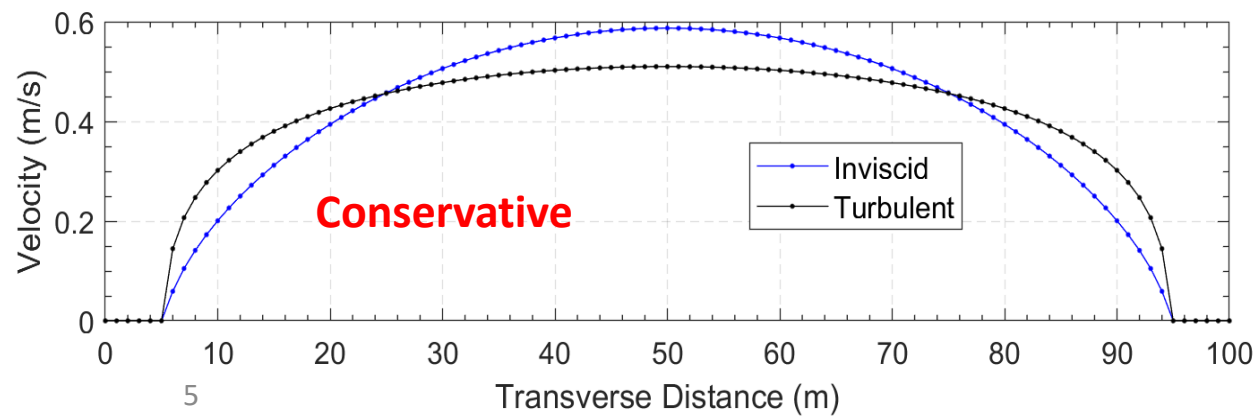
Mixing Term Formulation Comparison



Bathymetry and water level



Produces a net dissipation



Decreases velocities in middle of channel but increases velocities near banks



Eddy Viscosity: Turbulence Model

- Old: Parabolic $v_t = Du_*h$
 - Versions 5.0.7 and earlier
 - Isotropic (same in all directions)
 - 1 parameter: mixing coefficient D
- New: Parabolic-Smagorinsky

u_* : Shear velocity

h : Water depth

D : Mixing coefficient

D_L : Longitudinal mixing coefficient

D_T : Transverse mixing coefficient

C_s : Smagorinsky coefficient

$$v_t = \mathbf{D}u_*h + (C_s\Delta)^2 |\bar{S}|$$

$$|\bar{S}| = \sqrt{2\left(\frac{\partial u}{\partial x}\right)^2 + 2\left(\frac{\partial v}{\partial y}\right)^2 + \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}\right)^2} \quad \mathbf{D} = \begin{bmatrix} D_{xx} & 0 \\ 0 & D_{yy} \end{bmatrix} \quad \begin{aligned} D_{xx} &= D_L \cos^2 \theta + D_T \sin^2 \theta \\ D_{yy} &= D_L \sin^2 \theta + D_T \cos^2 \theta \end{aligned}$$

- Default method in Version 6.0
- Non-Isotropic (not the same in all directions)
- 3 parameters: D_L , D_T , and C_s

Turbulence Numerical Implementations

- Non-conservative mixing
 - Eulerian-Lagrangian Solver

$$\frac{u_N^{n+1} - u_N^*}{\Delta t} = -g \frac{\partial H^{n+\theta}}{\partial N} + v_t^n (\Delta u_N^n)_X - c_f u_N^{n+1}$$

Eulerian-Lagrangian

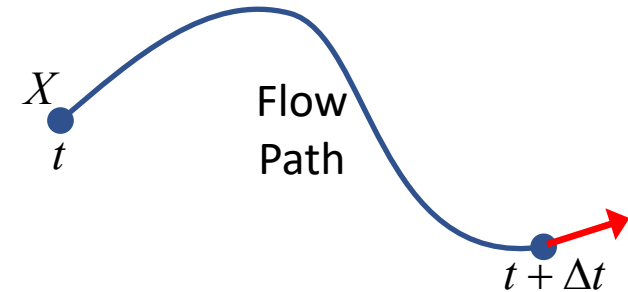
- All mixing terms explicit
- Approximate Stability Criteria for Eulerian Solver

$$\frac{v_t \Delta t}{\Delta x^2} \leq \frac{1}{2}$$

- Conservative mixing
 - Eulerian-Lagrangian Solver

$$\frac{u_N^{n+1} - u_N^*}{\Delta t} = -g \frac{\partial H^{n+\theta}}{\partial N} + \left[\frac{1}{h^n} \nabla \cdot (v_t^n h^n \nabla u_N^n) \right]_X - c_f u_N^{n+1}$$

Lagrangian



- Eulerian Solver

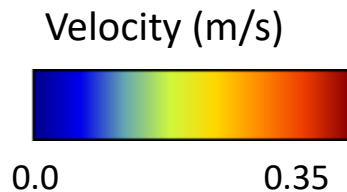
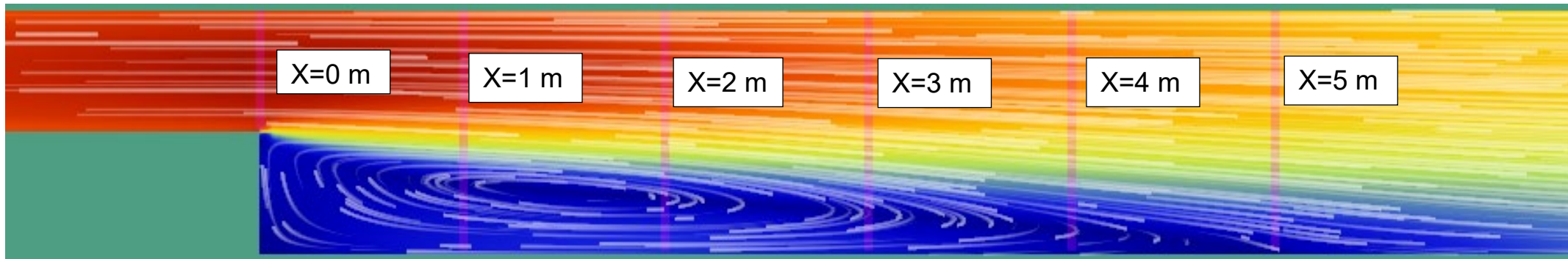
$$\frac{u_N^{n+1} - u_N^n}{\Delta t} + (V \cdot \nabla) u_N^n - f u_T^n = -g \frac{\partial H^{n+\theta}}{\partial N} + \frac{1}{h^n} \nabla \cdot (v_t^n h^n \nabla u_N^n) - c_f u_N^{n+1}$$

Eulerian



Example: Sudden Expansion Lab Experiment

- Inflow: $0.039 \text{ m}^3/\text{s}$
- Downstream depth: 11 cm
- Slope: 0.0001
- Grid Resolution: 2.5 cm
- Time step: 0.02 and 0.0333 s
- Manning's n: $0.015 \text{ s/m}^{1/3}$



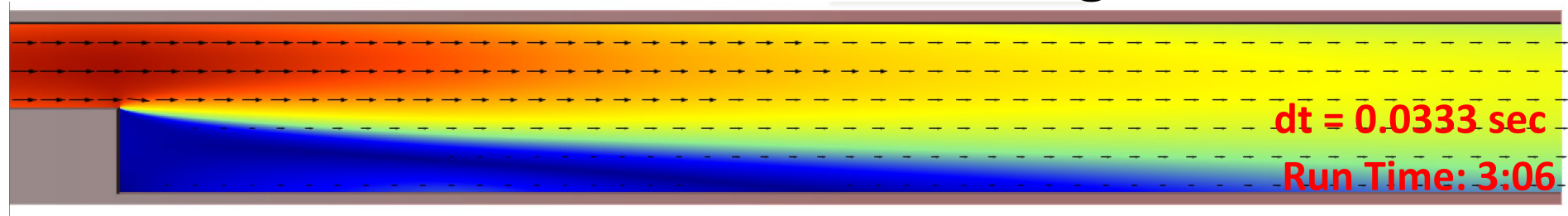


Results: Sudden Expansion Lab Experiment

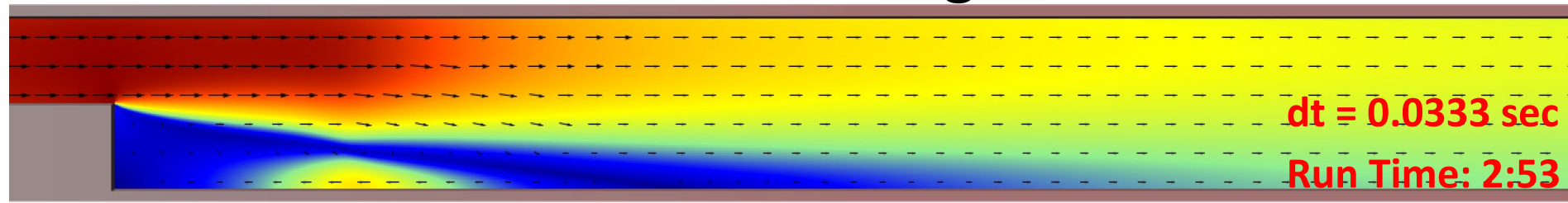


ELM Solver

Non-conservative Mixing



Conservative Mixing



$$D = 1.4$$

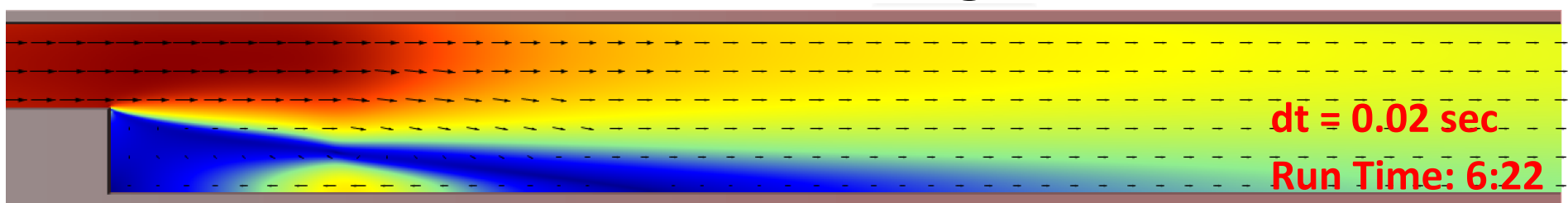
$$D_L = 0.6$$

$$D_T = 0.3$$

$$C_s = 0.1$$

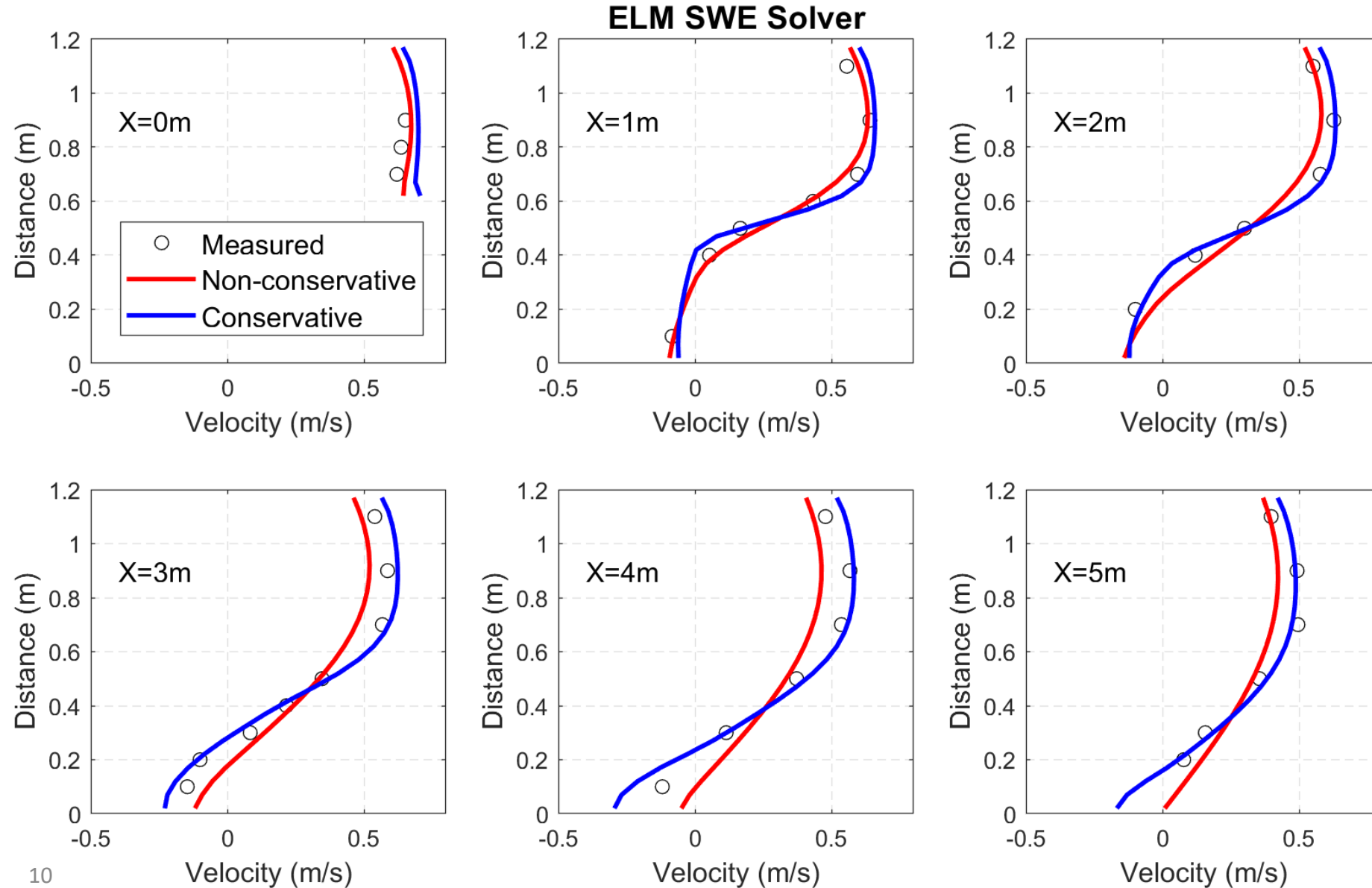
EM Solver

Conservative Mixing





Results: Sudden Expansion Lab Experiment





Turbulence Coefficients

- Best to calibrate coefficients with velocity measurements
- Non-conservative formulation generally requires larger values (2x) compared to the conservative formulation
- If coefficients are too large, the non-conservative formulation can produce excess dissipation and increase water levels
- When calibrating, start on the low end of the range

Mixing Intensity	Geometry and Surface	D_L	D_T
Weak	Straight channel Smooth Surface	0.1 to 0.3	0.04 to 0.1
Moderate	Gentle meanders Moderately irregular	0.3 to 1	0.1 to 0.3
Strong	Strong meanders Rough surface	1 to 3	0.3 to 1

Smagorinsky Coefficient: 0.05 to 0.2



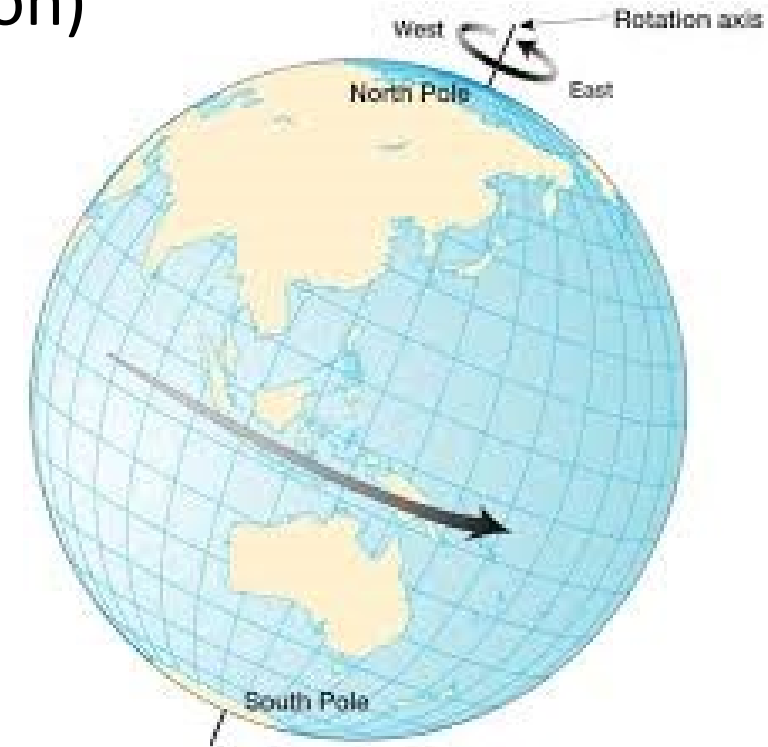
Discussion and Conclusions

- Non-conservative formulation
 - Does not conserve momentum
 - Will generally lead to a net dissipation of momentum
 - Still an option in Version 6.0 for backwards compatibility
- Conservative formulation
 - Conserves momentum
 - Recommended approach for both EM and ELM solvers
 - Generally requires smaller mixing coefficients than the non-conservative formulation
 - EM Solver has a time step restriction
 - ELM solver does not have a time step restriction
 - EM and ELM solvers should produce similar results for most cases



Coriolis Acceleration

- Effect of rotating frame of reference (earth's rotation)
- Constant for the each 2D domain (f-plane approx.)
$$f = 2 \omega \sin \varphi$$
 - ω : sidereal angular velocity of the Earth
 - φ : latitude. Positive for northern hemisphere. Negative for southern hemisphere
- Coriolis acceleration disabled by default to save computational time
- Negligible for most river and flood simulations
- When to enable Coriolis term?
 - Large domains
 - Higher latitudes





Coriolis Numerical Implementations



- Eulerian-Lagrangian Solver
 - Fractional Step Method (Semi-implicit)

$$\begin{pmatrix} 1 & \theta \Delta t f \\ \theta \Delta t f & 1 \end{pmatrix} \begin{pmatrix} u^* \\ v^* \end{pmatrix} = \begin{pmatrix} u_X^n + (1 - \theta) \Delta t f v_X^n \\ v_X^n + (1 - \theta) \Delta t f u_X^n \end{pmatrix} \quad \mathbf{V}^* = \begin{pmatrix} u^* \\ v^* \end{pmatrix}$$

f : Coriolis Parameter

θ : Implicit weighting factor

Δt : Time step interval

u_X^n : Backtracking velocity

$$\frac{u_N^{n+1} - u_N^*}{\Delta t} = -g \frac{\partial H^{n+\theta}}{\partial N} - c_f u_N^{n+1} \quad u_N^* = \mathbf{n}_f \cdot \mathbf{V}^*$$

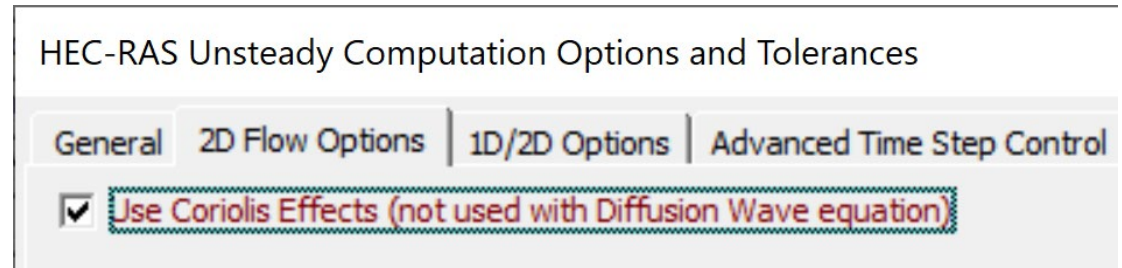
- Eulerian Solver
 - Explicit

$$\frac{u_N^{n+1} - u_N^n}{\Delta t} + (\mathbf{V} \cdot \nabla) u_N^n - f u_T^n = -g \frac{\partial H^{n+\theta}}{\partial N} - c_f u_N^{n+1}$$



Coriolis Discussion and Conclusions

- Only for Shallow Water Equations (Not Diffusion-Wave Equation)
- Relatively inexpensive
- Does not impact stability or introduce time step limitations
- When in doubt, turn it on
- Requires one input parameter:
average latitude for each 2D area
- Also requires checking a box

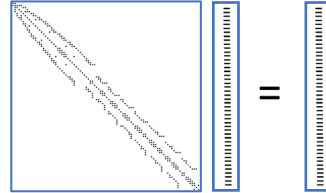




Matrix Solvers: Introduction

- Linear System of Equations

$$Ax = b$$



- Direct Solvers

- Examples: Gaussian elimination, LU, Cholesky, and QR decompositions
- Can be “black boxes”
- Usually have few input parameters
- High-accuracy
- Can fail or be very slow for large matrices
- Can be slow for unsteady or non-linear systems

- Iterative Solvers

- Examples: GS, SOR, CG, GMRES
- Require more options and input parameters
- Usually require preconditioners, matrix balancing, ordering, etc.
- Less accurate
- Good for large problems
- Good for unsteady or non-linear systems
- Improper use can lead to instability problems or solution divergence



HEC-RAS Direct Solver

- PARDISO

High-performance, robust, memory efficient and easy-to-use solver for symmetric and non-symmetric linear systems.

- Version in Intel Math Kernel Library
- Parallel on PC's
- Can be used as a “black box”.
 - Very little parameters
 - No need matrix balancing, ordering, etc.



HEC-RAS Iterative Solvers

- **SOR: Successive Over-Relaxation**
 - Relaxation factor ($0 < \omega < 2$)
 - Asynchronous (ASOR) parallel implementation
 - Extremely simple
 - May take many iterations to converge but each iteration is very inexpensive
- **FGMRES-SOR: Flexible Generalized Minimal RESidual**
 - “Flexible” variant of GMRES which allows preconditioner to vary from iteration to iteration
 - SOR as preconditioner



Iterative Solver Input Parameters

- **Convergence Tolerance**
 - Determines the overall accuracy
- **Minimum Iterations**
 - Increases accuracy, avoids solution drift, and allows the solver to stabilize
- **Maximum Iterations**
 - Avoids stalling and too many iterations caused by a small convergence tolerance
- **Restart Iteration (Only FGMRES-SOR)**
 - Reduces run time and memory requirements
- **Relaxation Factor**
 - Used for both SOR solver and preconditioner
- **SOR Preconditioner Iterations (Only FGMRES-SOR)**
 - In-lieu of checking convergence which would be slower

Parameter	Range
Convergence Tolerance	0.001 – 0.000001
Minimum Iterations	3 – 6
Maximum Iterations	5 – 30
Restart Iteration (FGMRES Only)	8 – 12
Relaxation Factor	1.1 – 1.5
SOR Preconditioner Iterations (FGMRES Only)	5 – 20



Iterative Solvers: Stopping Criteria

- Error Estimate

$$E^m = \frac{\|D^{-1}(Ax^m - b)\|_2}{\sqrt{N}}$$

D : Diagonal of A

A : Coefficient matrix

x : Solution

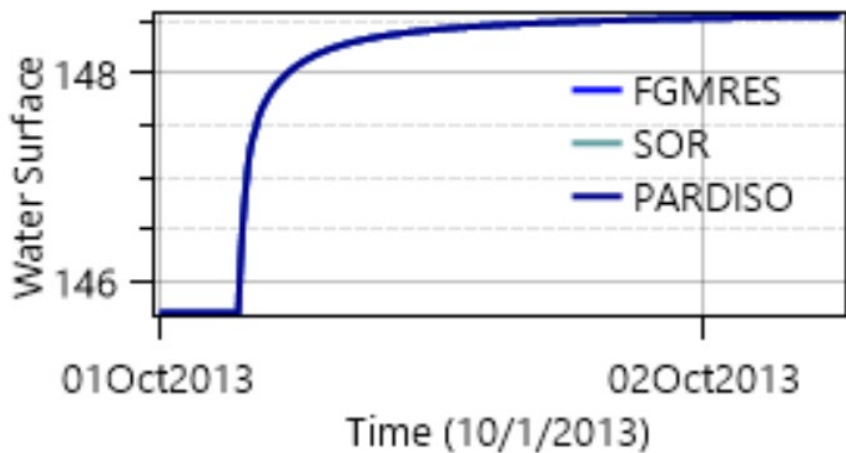
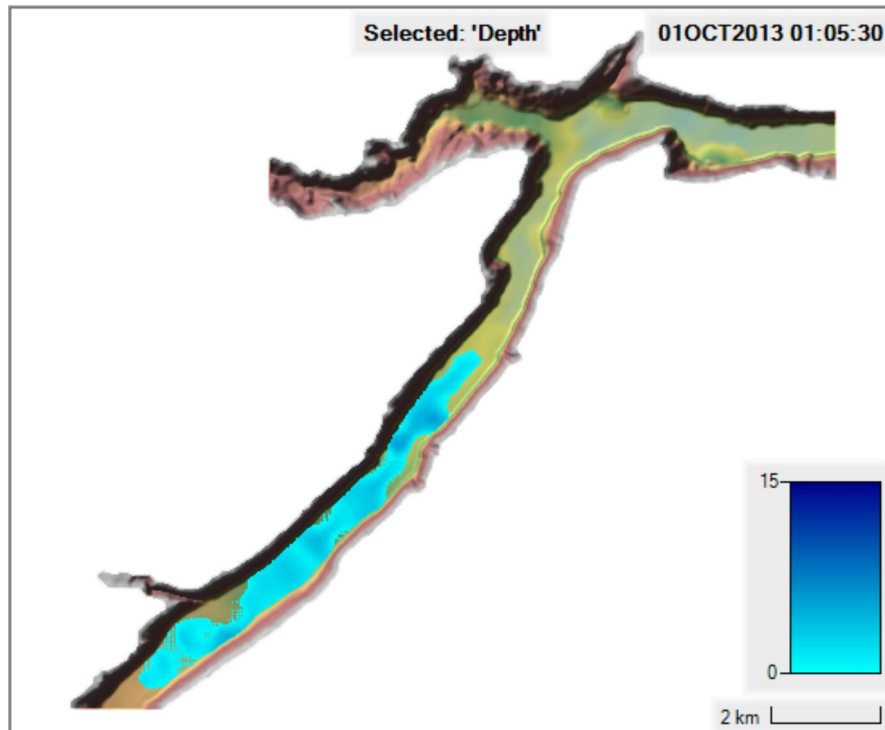
b : Right-hand-side

N : Number of rows

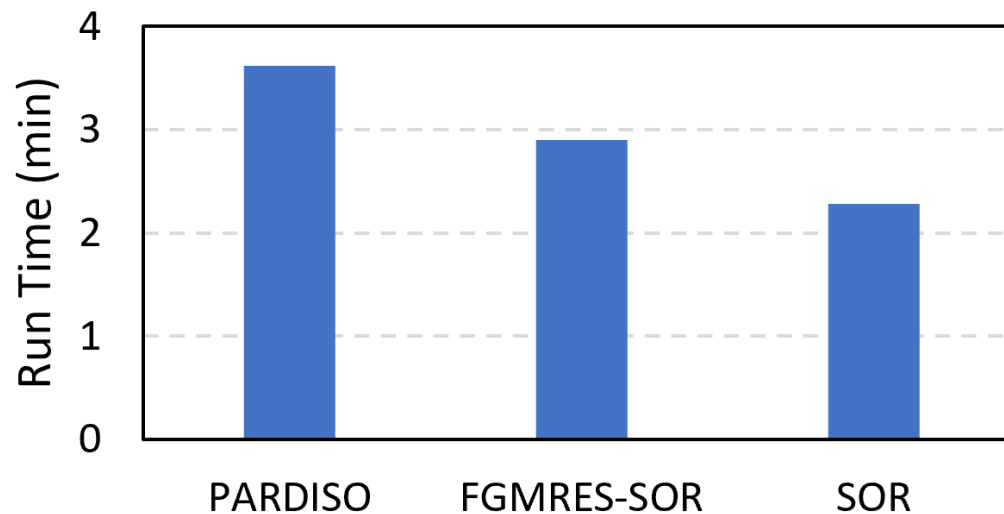
Iterative Solver Status	Criteria	Description
Iterating	$N_{\min} < m < N_{\max}$ and $E^m > T_C$ and $\frac{E^{m-1} - E^m}{E^1 - E^m} > T_S$ and $E^m < E^1$	Iterative solver is converging and will continue to iterate. N_{\min} : Minimum number of iterations N_{\max} : Maximum number of iterations T_C : Convergence tolerance $T_S = 0.1T_C$: Stalling tolerance
Converged	$E^m \leq T_C$	Convergence criteria met. Solution accepted.
Stalled	$\frac{E^{m-1} - E^m}{E^1 - E^m} \leq T_S$	Convergence rate has decreased to an insignificant level without satisfying the converged criteria. The current solution is accepted and the iteration loop is exited.
Max Iterations	$m = N_{\max}$	Maximum number of iterations reached without reaching the converged criteria. The current solution is accepted and the iteration loop is exited.
Divergent	$E^m > E^1$	Iterative solution is divergent. Either the normalized residuals are getting larger, or a Not a Number (NaN) has been detected.



Example: EA Test 5 (Dam Failure)



Setting	FGMRES-SOR	SOR
Convergence Tolerance	0.0001	0.0001
Minimum Iterations	3	5
Maximum Iterations	20	30
Restart Iteration	10	
Relaxation Factor	1.3	1.3
SOR Preconditioner Iterations	10	





Matrix Solver Best Practices

- Start with PARDISO
- Ensure model is stable and not going to max iterations every time step or reporting large water surface or volume errors
- Try FGMRES and SOR solvers
- Start with conservative parameters
- Compare with PARDISO
- Adjust parameters to optimize run time
- Iteration parameters left empty or set to zero are assigned a default value based on mesh size

Thank You!

HEC-RAS Website:

<https://www.hec.usace.army.mil/software/hec-ras/>

Online Documentation:

<https://www.hec.usace.army.mil/confluence/rasdocs>