#### What's New with HEC-RAS 5.1

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## Major New Hydraulics Features for HEC-RAS 5.1

- Spatial Precipitation
- Spatial Infiltration
- Wind Forces
- 1D Finite Volume solver
- New 2D full momentum solver with greater Momentum conservation properties
- Pump stations inside 2D Flow Areas
- ID Bridge Hydraulics inside 2D Flow Areas
- Computational speed improvements
- 3D Visualization tool

## **Spatial Precipitation**

#### Gridded Data

- HEC-DSS file format (from HEC-MetView)
- GRIB NWS
- NetCDF NWS

#### Point Gage Data

- HEC-DSS time series
  - Regular Interval
  - Irregular Interval
- User Entered into a Table

## **Unsteady Flow Boundary Conditions**

File Options Help Description Wind Forces: No Wind Forces Air Density: Standard Meteorological Stations (required for point time series data) View/Edit Stations Plot Stations Plot Stations Precipitation Mode: Gridded Point Source Constant DSS Data Filename: C:\HEC Data\HEC:RAS\Automated Test Datasets 51\2D Unsteady Flow Hydraulics\ Path: /SHG/MARFC/PRECIP/01SEP2018:0200/01SEP2018:0300/NEXRAD/ Projection Override (Optional): Mint Description Projection Override (Optional): Mint Description Projection Override (Optional): Mint Description Projection Override (Optional): Mint Projection Ove	1 Unsteady Flow Data - Gridded Precipitation -	×
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## Gridded Data

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## Gridded Precipitation example HEC-RAS

## Point Gage Data

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Det	ailed View Summary	View					
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	Station Name	Height	Project X	Project Y	Longitude	Latitude	
	ALVIN BUSH DAM	2	1922740.6	431189.94	-77.9166667	41.3	
	DRIFTWOOD	2	1863234.88		-78.1333333	41.3383333	
3	HOLLIDAYSBURG 2	2	1790610.4	95591.73	-78.3888889	40.4272222	2
4	MILROY 2 WNW	2	2012703.14	199422.25	-77.5905556	40.7138889	9
5	PHILIPSBURG 8 E	2	1838408.6	266227.39	-78.2205556	40.8963889	9
6	RAYSTOWN LAKE 2	2	1896963.52	97268.31	-78.0069444	40.4333333	3
7	TYRONE	2	1832952.79	183975.72	-78.2386111	40.6705556	5
8	WILLIAMSPORT RGNL	2	2197049.88	394058.28	-76.9188889	41.2452	2
9	CRESSON 1 SE	2	1734232.01	104373.03	-78.5916667	40.45	5
10	CURWENSVILLE LAKE	2	1786461.52	322534.71	-78.41	41.0	5
11	DU BOIS 7 E	2	1690689.7	349266.08	-78.7583333	41.1208333	3
	MADERA 2 SE	2	1778927.51	241828.17	-78,435	40.8283333	
	MILLHEIM	2	2044073.29	263969.12	-77.4766667	40.8908333	
	RENOVO 6 S	2	1968271.12	422543.08	-77.7508333	41.326388	
	SAYERS DAM	2	2007191.2	321872.44		41.0	
	STATE COLLEGE	2	1943600.61	248985.51	-77.84	40.8	
						Cancel	
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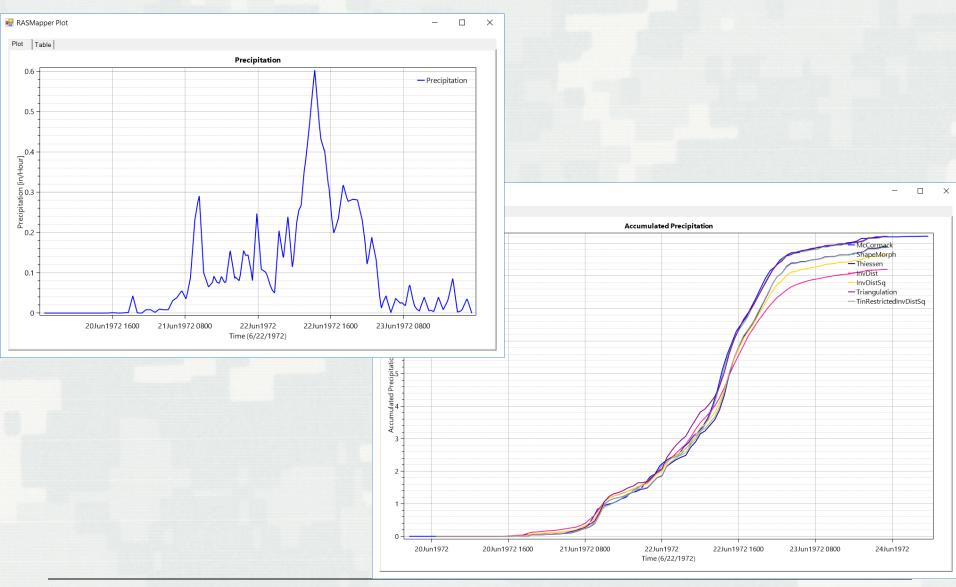
## Point Gage Data

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ile Options Help	
Description	Apply Data
Boundary Conditions   Initial Conditions   Meteorological Data	
Precipitation: Use Precipitation  Wind Forces: No Wind Forces  Air Density: Standard	-
Meteorological Stations (required for point time series data)         View/Edit Stations         Plot Stations	
Meteorological Variables Precipitation	
Mode: Point  Ratio (Optional): Point Time Series Mode (Nearest)	
1       ALVIN BUSH DAM       Inverse Distance       o       0.500 (inches)          2       CRESSON 1 SE       Inverse Distance Squared       o       0.470 (inches)          3       CURWENSVILLE L       Triangulation       o       0.300 (inches)          4       DRIFTWOOD       Peak Preservation       o       0.390 (inches)          5       DU BOIS 7 E       Shape Preservation       o       0.510 (inches)          6       HOLLIDAYSBURG 2       Laplace       0.000 (inches)	

## **Cumulative Rainfall**



## **Rainfall Time Series Plots**



## **Spatial Infiltration**

#### Three Methods

- Deficit Constant method
- SCS Curve Number
- Green and Ampt
- Spatial Data
  - Soils
  - Land cover

#### Other Optional Data

- Evapotranspiration
- Mean Monthly Pan evaporation data

## Wind Forces

Added to 1D and 2D solution algorithms

- 1D Finite Difference and 1D Finite Volume SWE
- 2D SWE current and new equation solver.
- Not in 2D Diffusion Wave solver

#### **1D Momentum Equation**

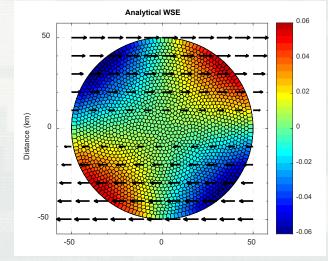
$$\frac{\partial Q}{\partial t} + \frac{\partial (VQ)}{\partial x} + gA\left(\frac{\partial \eta}{\partial x} + S_f + S_h\right) = T_w \frac{\tau_{sh}}{\rho_w}$$

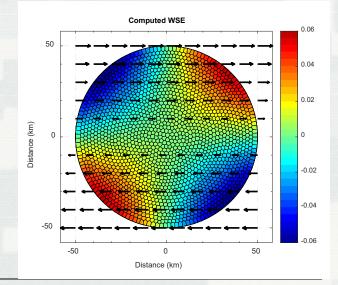
#### Data Sources

- Gridded Data
- Gaged Point data
- User Entered Table

## Wind Verification

- Flat circular basin
- Spatially variable wind forcing in the x-direction only
- Linear bottom friction
- Polygonal mesh





## Wind Application - Animation

## Wind 1D Profile Animation

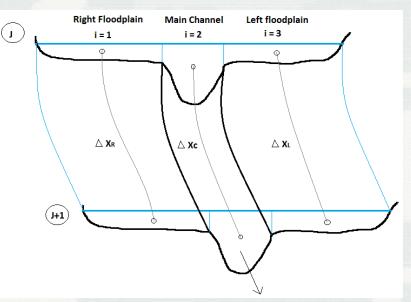
## 1D Finite Volume Solution Algorithm

# The new 1D Finite Volume algorithm has the following positive attributes:

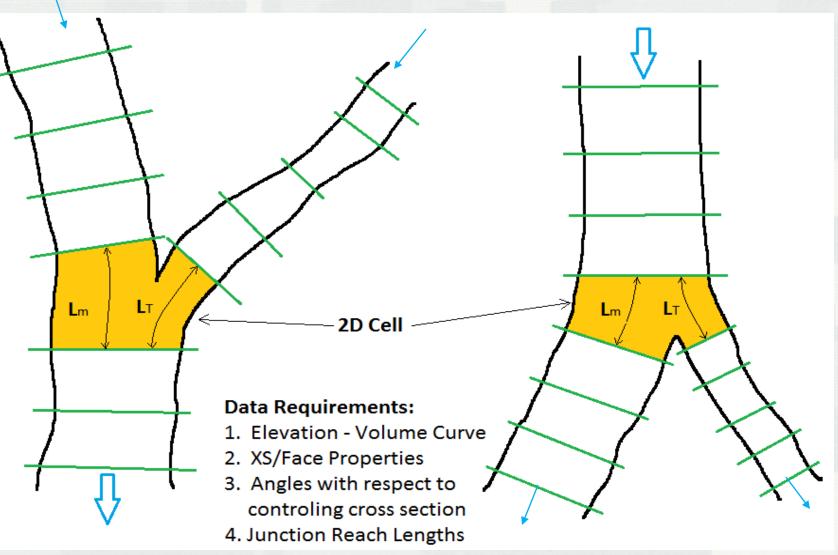
- Can start with channels completely dry, or they can go dry during a simulation (wetting/drying)
- Very stable for low flow modeling
- Can handle extremely rapidly rising hydrographs without going unstable
- Handles subcritical to supercritical flow, and hydraulic jumps better – No special option to turn on.
- Junction analysis is performed as a single 2D cell when connecting 1D reaches (continuity and momentum is conserved through the junction)

#### Partial Cells Left floodplain, Main channel, Right floodplain

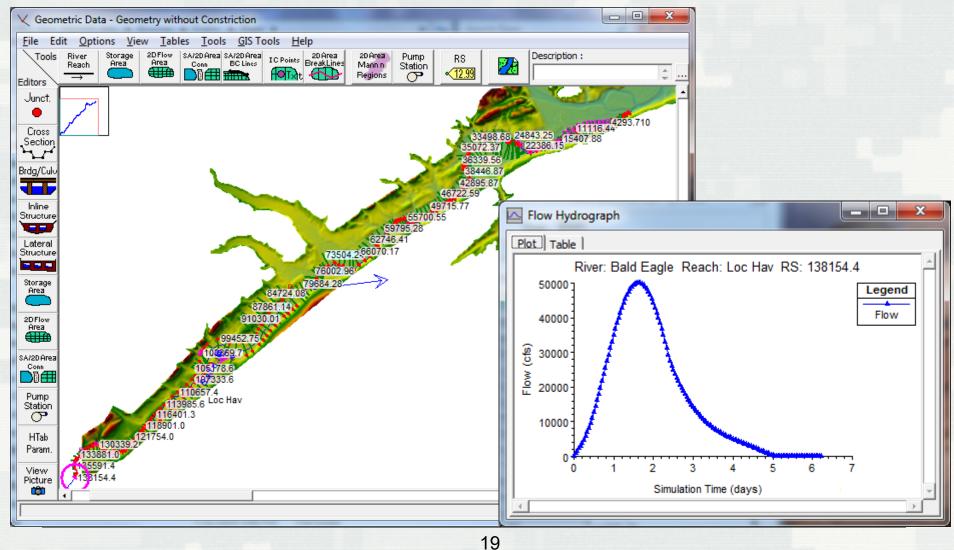
- Separate cells for main channel, left floodplain and right floodplain.
- Current Finite Difference uses only two flow areas: channel & floodplain
- Notation: Partial cells indexed by *i*
- $u_{ji}$  = channel or overbanks velocities at
- $A_{ji}$  = channel or overbanks partial areas for cross-section *j*
- $A_j = \sum_i A_{ji}$  cross-section total area
- Cross-section partial conveyance  $K_{ji} = (A_{ji}R_{ji}^{2/3})/(n_{ji}/k)$
- Cross-section total conveyance  $K_j = \sum_i K_{ji}$



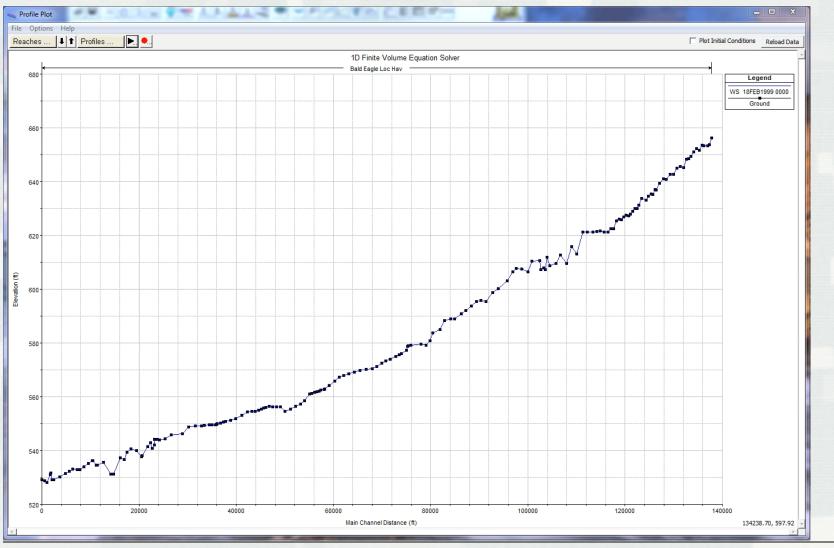
## Junctions



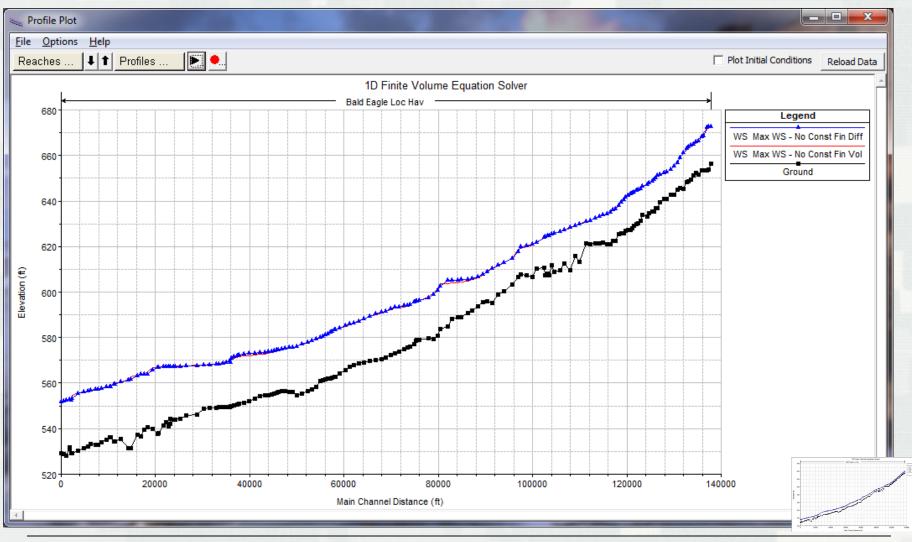
# Natural River – No Connections Starting Dry, then wet, then dry



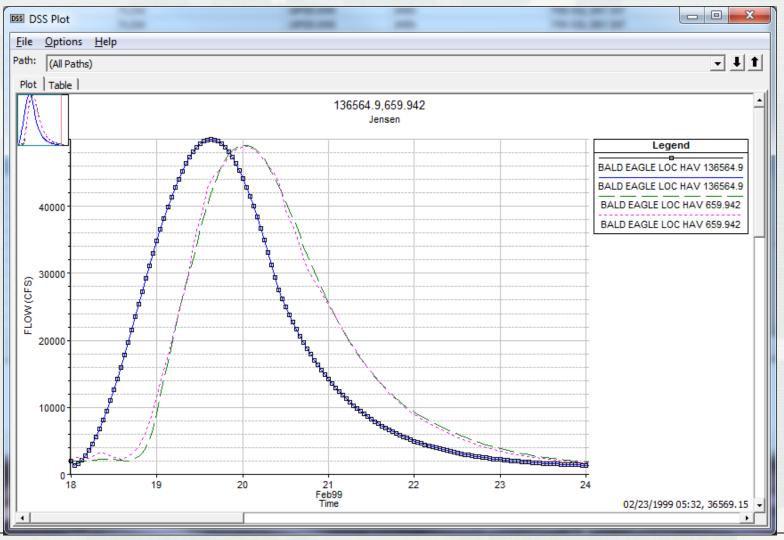
#### Natural River — Continued Animation - Finite Volume - Dry to Wet to Dry



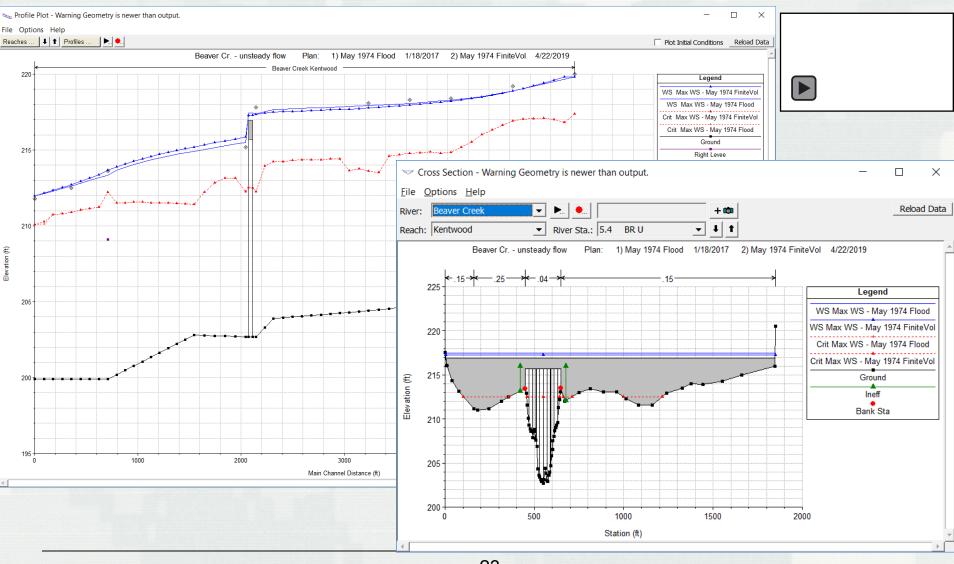
#### Natural River — Continued Finite Volume vs Finite Difference – Starting Wet



#### Natural River — Continued Upstream Inflow and Downstream Outflows



## **1D Bridge Hydraulics Beaver Creek**

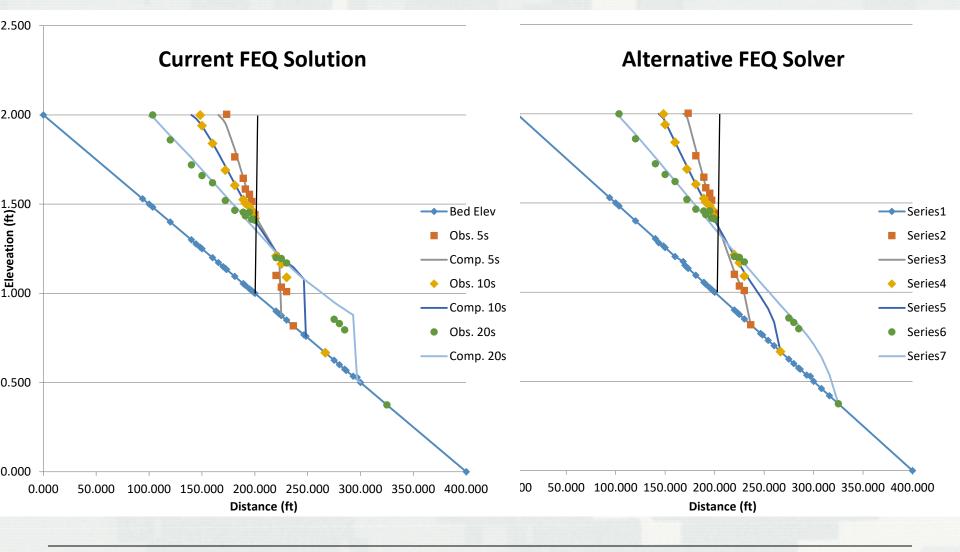


## **Bald Eagle Creek with Bridges**

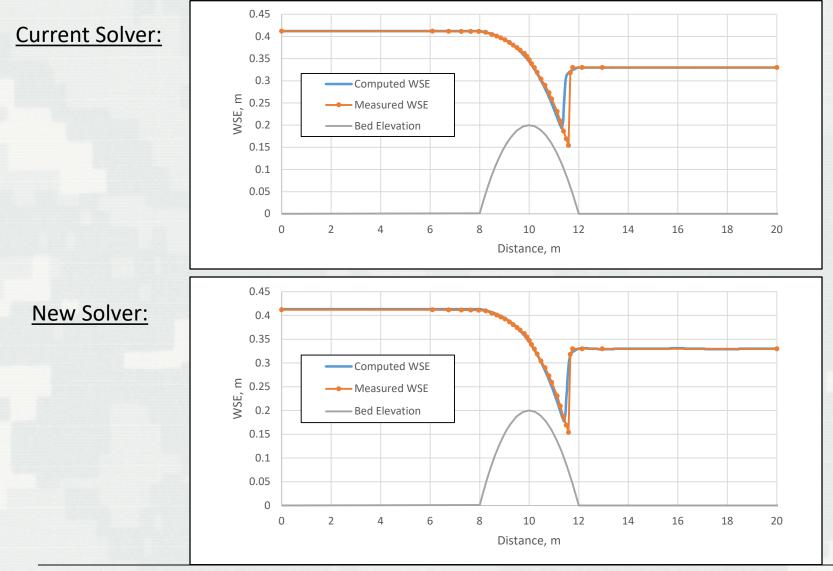
## Alternative Solution Scheme for Shallow Water Equations

- Momentum conservative discretization of the acceleration terms
  - Greater momentum conservation than current solver in current version
- Semi Explicit Time step is somewhat limited by the Courant condition
  - Generally requires smaller time steps and more computational time to run

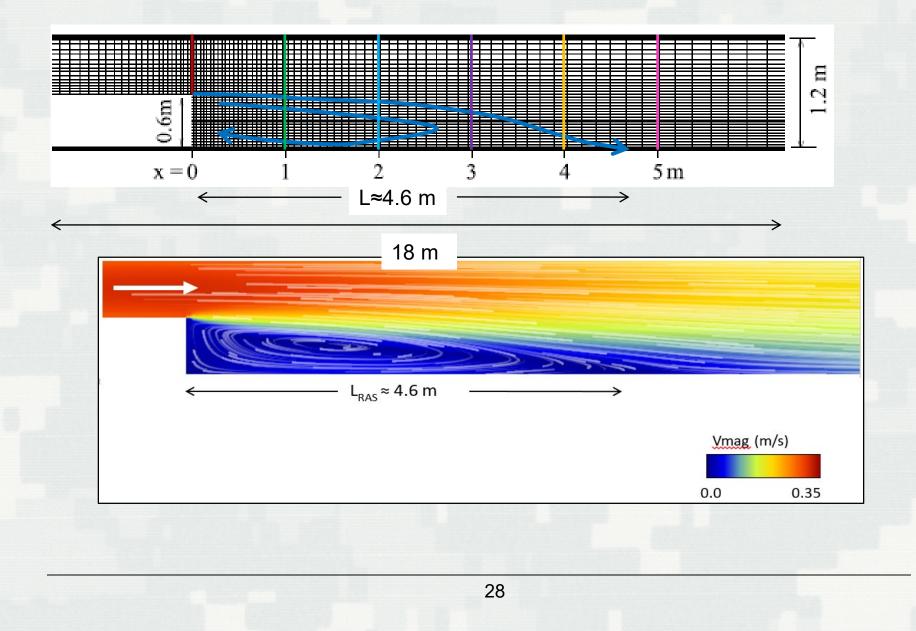
#### Sudden Dambreak in a Flume (WES Data Set and report from 1960)



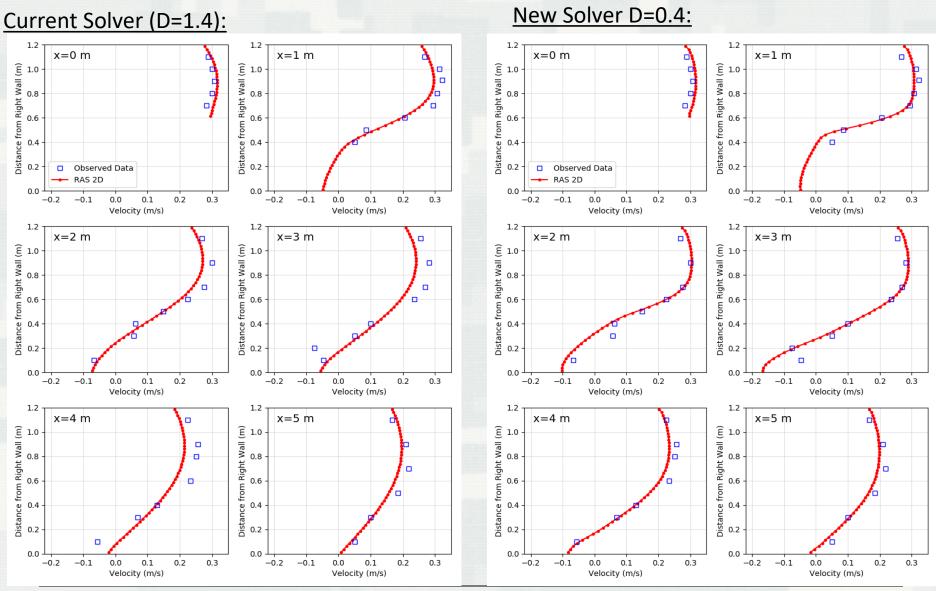
#### Flow over a Bump assuming no Friction



#### Sudden Expansion – Lab Data



#### **Sudden Expansion**





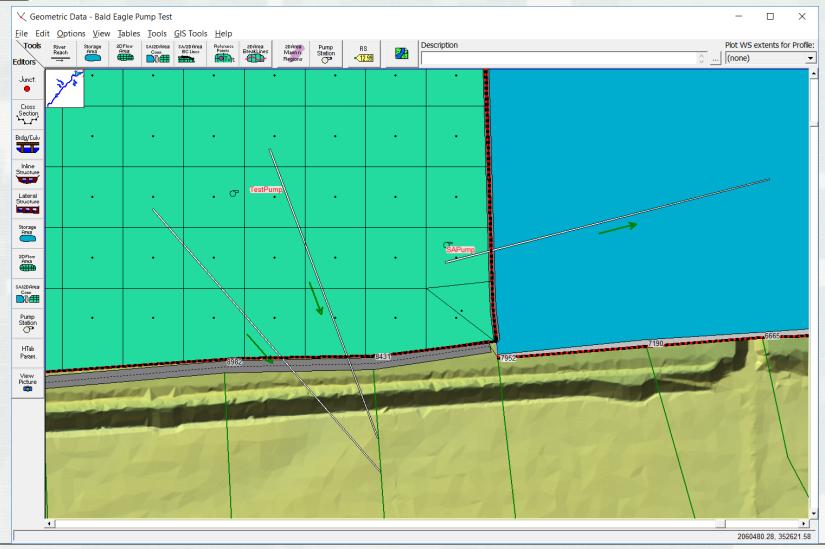
## Pump Stations Connected to 2D Flow Areas

- Pump Stations now how spatial connections
  - X, Y coordinates for too and from locations
- Can now connect to 2D flow areas
  - 2D cell to another 2D cell
  - 2D cell to Storage Area
  - 2D cell to 1D river reach (XS location)

## **Pump Stations Example**

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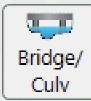
Pump Station





## **Pump Stations Example**

Pump Group: G	×
Selected Layer Depth	
<ul> <li>Belle Conditions</li> <li>Casemetries</li> <li>Casemetries<td></td></li></ul>	
Image: Construction of the construc	
<ul> <li>Event Conditions</li> <li>Geometry</li> <li>Opepth (Mex)</li> <li>Velocity (01JAN1999 12:00:00)</li> <li>WSE (03JAN1999 20:30:00)</li> <li>Moe LandUse</li> <li>Main ChannelBanks</li> <li>USGS Imagery</li> <li>Google Hybrid</li> <li>stret100k_1_p0035</li> <li>NLCD 2016 Land Cover L48 20190-</li> <li>NLCD 2016 Land Cover L48 20190-</li> </ul>	ata Editor         me:       UpTheHill         Image: UpTheHill       Image: UpTheHill <t< td=""></t<>
32 Plot Pump Efficie	ciency Curves OK Cance



## 1D Bridge Hydraulics inside of a 2D Flow Area

- Develop a family of Headwater Tailwater Flow curves from 1D bridge hydraulic calculations
- Option to compute flow over the top of the bridge as weir flow or normal 2D flow equations
- Flows through the bridge opening will take into account momentum transfer
  - Flow and Velocity Boundary condition

## **Computational Speed Improvements**

#### New Matrix Format

- Previous versions allowed the matrix to be Non-Symmetric
- Version 5.1 uses a Symmetric matrix format
- This allowed us to use a faster solver Symmetric Positive Definite Solver

#### Boundary Condition Cells

- Previous version had B.C. cells along entire boundary of 2D area
  - Done for simplicity and consistency (.i.e. keep the code simple)
- Version 5.1 only has extra cells a user defined boundary condition locations
  - Fewer cells means less computations Faster solution

## 5.0.7 vs 5.1 2D Computational Speed

2D Test Name	Number Cells	Equation Type	5.0.7	5.1	Speed Factor
Bald Eagle Detailed	87,022	FEQ	1 hr 29 min 55s	59 min 37s	1.51
Muncie 2D 50ft Grid	5,376	FEQ	1 min 15s	55s	1.36
Saint Paul 2D	2,251	Diff	1 min 32s	1 min 01s	1.51
EU Test No 2	10,000	FEQ	40s	22s	1.82
EU Test No 4	80,000	FEQ	56s	40s	1.40
EU Test No 5	7,460	FEQ	50s	36s	1.39
EU Test No 6	36,492	FEQ	1 min 18s	50s	1.56
EU Test No 7 20m grid	16,590	FEQ	12 min 25s	10 min 26s	1.19
EU Test 8A 2m grid	97,000	FEQ	1 hr 10 min 36s	48 min 26s	1.45
Yolo Bypass2	17,129	FEQ	9 min 34s	8 min 11s	1.17
Boise River	10,423	FEQ	10 min 46s	6 min 57s	1.55
Truckee River 1D/2D	162,805	Diff	1 hr 18 min 27s	47 min 6s	1.67
400 sq mi Watershed	2,033,190	Diff	16 hrs 45 min 14s	9 hrs 53 min 55s	1.69
Average Speed Increase					1.50

## **2D Iterative Matrix Solvers**

#### HEC-RAS 5.0.7 uses a solver called PARDISO - direct solver

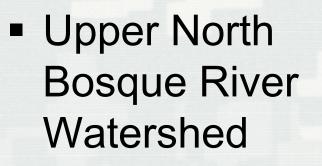
- Better for model stability and volume accounting
- Slower

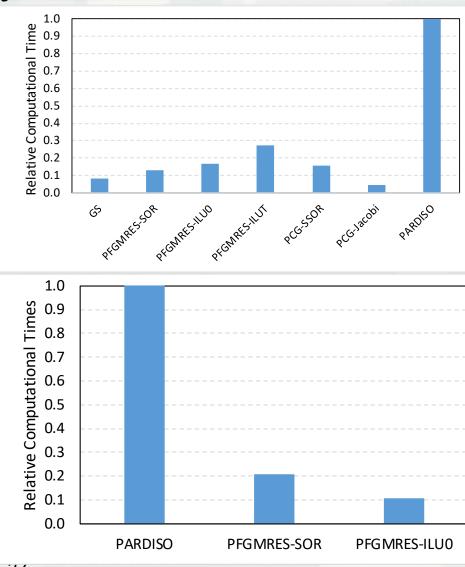
#### For HEC-RAS 5.1 we have added optional Iterative Solvers

- Potentially faster
- Requires user-based solution tolerance
- Potentially less stable

#### Iterative Matrix Solvers Note: Times are only for matrix solution

 Channel constriction and expansion





## 5.0.7 vs 5.1 with Iterative Solvers

2D Test Name	Number Cells	Equation Type	5.0.7	5.1	5.1 Iter Solv	Speed Factor
Bald Eagle Detailed	87,022	FEQ	1 hr 29 min 55s	59 min 37s	51 min 47s	1.73
Muncie 2D 50ft Grid	5,376	FEQ	1 min 15s	55s	51s	1.47
Saint Paul 2D	2,251	Diff	1 min 32s	1 min 01s	1 min 52s	0.82
EU Test No 2	10,000	FEQ	40s	22s	13s	3.08
EU Test No 4	80,000	FEQ	56s	40s	25s	2.24
EU Test No 5	7,460	FEQ	50s	36s	24s	2.08
EU Test No 6	36,492	FEQ	1 min 18s	50s	37s	2.11
EU Test No 7 20m grid	16,590	Diff	12 min 25s	10 min 26s	6 min 57s	1.79
EU Test 8A 2m grid	97,000	FEQ	1 hr 10 min 36s	48 min 26s	15 min 2s	4.69
Yolo Bypass2	17,129	FEQ	9 min 34s	8 min 11s	5 min 41s	1.68
Boise River	10,423	FEQ	10 min 46s	6 min 57s	4 min 50s	2.23
Truckee River 1D/2D	162,805	Diff	1 hr 18 min 27s	47 min 6s	1 hr 10 min 30s	1.1
400 sq mi Watershed	2,033,190	Diff	16 hrs 45 min 14s	9 hrs 53 min 55s	11 hr 3 mins 43s	1.52
Average Speed Increase						2.04

## **3D Visualization tool**

